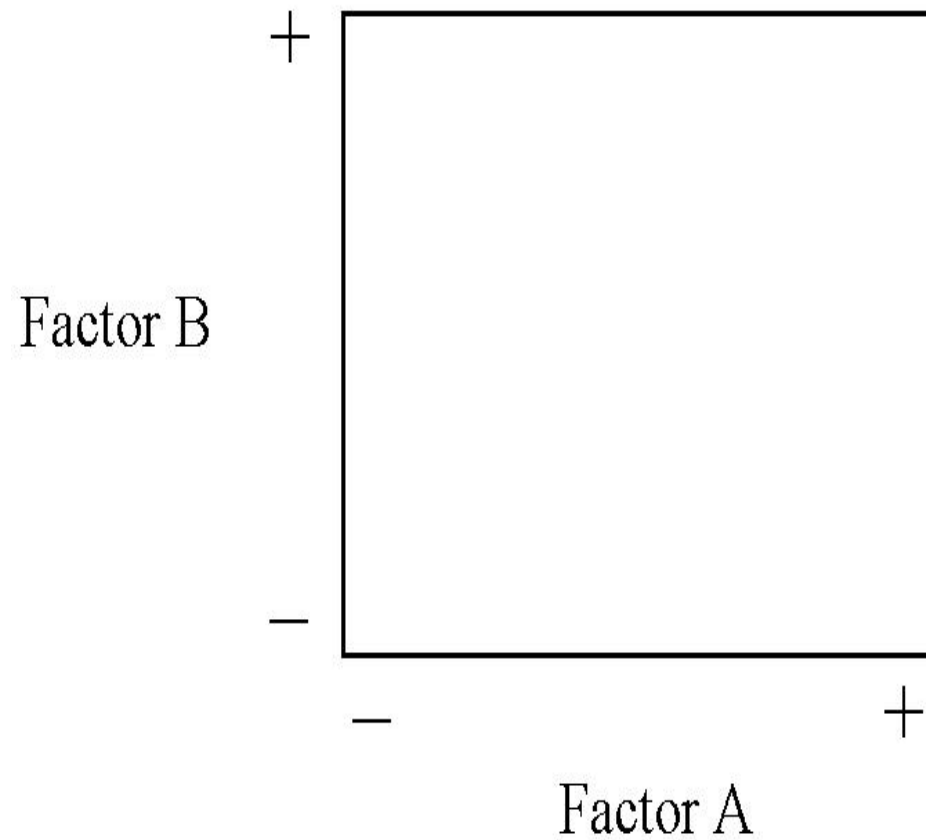


## **Lecture 9: Factorial Design**

Montgomery: chapter 5

## Examples

Example I. Two factors (A, B) each with two levels ( $-$ ,  $+$ )



## Three Data for Example I

Ex.I-Data 1

B	A	
	—	+
+	27,33	51,51
—	18,22	39,41

EX.I-Data 2

B	A	
	—	+
+	38,42	10,14
—	19,21	53,47

EX.I-Data 3

B	A	
	—	+
+	27,33	62,68
—	21,21	38,42

**Example II: Battery life experiment**

An engineer is studying the effective life of a certain type of battery. Two factors, plate material and temperature, are involved. There are three types of plate materials (1, 2, 3) and three temperature levels (15, 70, 125). Four batteries are tested at each combination of plate material and temperature, and all 36 tests are run in random order. The experiment and the resulting observed battery life data are given below.

material	temperature		
	15	70	125
1	130,155,74,180	34,40,80,75	20,70,82,58
2	150,188,159,126	136,122,106,115	25,70,58,45
3	138,110,168,160	174,120,150,139	96,104,82,60

### **Example III: Bottling Experiment**

A soft drink bottler is interested in obtaining more uniform fill heights in the bottles produced by his manufacturing process. An experiment is conducted to study three factors of the process, which are

the percent carbonation (A): 10, 12, 14 percent

the operating pressure (B): 25, 30 psi

the line speed (C): 200, 250 bpm

The response is the deviation from the target fill height. Each combination of the three factors has two replicates and all 24 runs are performed in a random order. The experiment and data are shown below.

Carbonation(A)	pressure(B)			
	25 psi		30 psi	
	LineSpeed(C)		LineSpeed(C)	
	200	250	200	250
10	-3,-1	-1,0	-1,0	1, 1
12	0, 1	2,1	2,3	6,5
14	5,4	7,6	7,9	10,11

## Factorial Design

- a number of factors:  $F_1, F_2, \dots, F_r$ .
- each with a number of levels:  $l_1, l_2, \dots, l_r$
- number of all possible level combinations (treatments):  $l_1 \times l_2 \dots \times l_r$
- interested in (main) effects, 2-factor interactions (2fi), 3-factor interactions (3fi), etc.

**One-factor-a-time design** as the opposite of factorial design.

Advantages of factorial over one-factor-a-time

- more efficient (runsize and estimation precision)
- able to accommodate interactions
- results are valid over a wider range of experimental conditions

## Statistical Model (Two Factors: A and B)

- Statistical model is

$$y_{ijk} = \mu + \tau_i + \beta_j + (\tau\beta)_{ij} + \epsilon_{ijk} \quad \left\{ \begin{array}{l} i = 1, 2, \dots, a \\ j = 1, 2, \dots, b \\ k = 1, 2, \dots, n \end{array} \right.$$

$\mu$  - grand mean

$\tau_i$  -  $i$ th level effect of factor A (ignores B) (main effects of A)

$\beta_j$  -  $j$ th level effect of factor B (ignores A) (main effects of B)

$(\tau\beta)_{ij}$  - interaction effect of combination  $ij$  (Explain variation not explained by main effects)

$$\epsilon_{ijk} \sim N(0, \sigma^2)$$

- Over-parameterized model: must include certain parameter constraints. Typically

$$\sum_i \tau_i = 0 \quad \sum_j \beta_j = 0 \quad \sum_i (\tau\beta)_{ij} = 0 \quad \sum_j (\tau\beta)_{ij} = 0$$



## Estimates

- Rewrite observation as:

$$y_{ijk} = \bar{y}_{...} + (\bar{y}_{i..} - \bar{y}_{...}) + (\bar{y}_{.j.} - \bar{y}_{...}) + (\bar{y}_{ij.} - \bar{y}_{i..} - \bar{y}_{.j.} + \bar{y}_{...}) + (y_{ijk} - \bar{y}_{ij.})$$

- result in estimates

$$\hat{\mu} = \bar{y}_{...}$$

$$\hat{\tau}_i = \bar{y}_{i..} - \bar{y}_{...}$$

$$\hat{\beta}_j = \bar{y}_{.j.} - \bar{y}_{...}$$

$$\widehat{(\tau\beta)}_{ij} = \bar{y}_{ij.} - \bar{y}_{i..} - \bar{y}_{.j.} + \bar{y}_{...}$$

- predicted value at level combination  $ij$  is

$$\hat{y}_{ijk} = \bar{y}_{ij.}$$

- Residuals are

$$\hat{\epsilon}_{ijk} = y_{ijk} - \bar{y}_{ij.}$$

## Partitioning the Sum of Squares

- Based on

$$y_{ijk} = \bar{y}_{...} + (\bar{y}_{i..} - \bar{y}_{...}) + (\bar{y}_{.j.} - \bar{y}_{...}) + (\bar{y}_{ij.} - \bar{y}_{i..} - \bar{y}_{.j.} + \bar{y}_{...}) + (y_{ijk} - \bar{y}_{ij.})$$

- Calculate  $SS_T = \sum (y_{ijk} - \bar{y}_{...})^2$
- Right hand side simplifies to

$$SS_A : \quad bn \sum_i (\bar{y}_{i..} - \bar{y}_{...})^2 + \quad df = a - 1$$

$$SS_B : \quad an \sum_j (\bar{y}_{.j.} - \bar{y}_{...})^2 + \quad df = b - 1$$

$$SS_{AB} : \quad n \sum_i \sum_j (\bar{y}_{ij.} - \bar{y}_{i..} - \bar{y}_{.j.} + \bar{y}_{...})^2 + \quad df = (a - 1)(b - 1)$$

$$SS_E : \quad \sum_i \sum_j \sum_k (y_{ijk} - \bar{y}_{ij.})^2 \quad df = ab(n - 1)$$

- $SS_T = SS_A + SS_B + SS_{AB} + SS_E$
- Using  $SS/df$  leads to  $MS_A, MS_B, MS_{AB}$  and  $MS_E$ .

## Testing Hypotheses

- 1 Main effects of  $A$ :  $H_0 : \tau_1 = \dots = \tau_a = 0$  vs  $H_1$  : at least one  $\tau_i \neq 0$ .
- 2 Main effects of  $B$ :  $H_0 : \beta_1 = \dots = \beta_b = 0$  vs  $H_1$  : at least one  $\beta_j \neq 0$ .
- 3 Interaction effects of  $AB$ :

$$H_0 : (\alpha\beta)_{ij} = 0 \text{ for all } i, j \text{ vs } H_1 : \text{at least one } (\tau\beta)_{ij} \neq 0.$$

- $E(\text{MS}_E) = \sigma^2$

$$E(\text{MS}_A) = \sigma^2 + bn \sum \tau_i^2 / (a - 1)$$

$$E(\text{MS}_B) = \sigma^2 + an \sum \beta_j^2 / (b - 1)$$

$$E(\text{MS}_{AB}) = \sigma^2 + n \sum (\tau\beta)_{ij}^2 / (a - 1)(b - 1)$$

- Use F-statistics for testing the hypotheses above:

$$1: F_0 = \frac{SS_A / (a-1)}{SS_E / (ab(n-1))} \quad 2: F_0 = \frac{SS_B / (b-1)}{SS_E / (ab(n-1))} \quad 3: F_0 = \frac{SS_{AB} / (a-1)(b-1)}{SS_E / (ab(n-1))}$$

## Analysis of Variance Table

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	$F_0$
Factor A	$SS_A$	$a - 1$	$MS_A$	$F_0$
Factor B	$SS_B$	$b - 1$	$MS_B$	$F_0$
Interaction	$SS_{AB}$	$(a - 1)(b - 1)$	$MS_{AB}$	$F_0$
Error	$SS_E$	$ab(n - 1)$	$MS_E$	
Total	$SS_T$	$abn - 1$		

$$SS_T = \sum \sum y_{ijk}^2 - y_{...}^2 / abn; \quad SS_A = \frac{1}{bn} \sum y_{i..}^2 - y_{...}^2 / abn$$

$$SS_B = \frac{1}{an} \sum y_{.j.}^2 - y_{...}^2 / abn; \quad SS_{\text{subtotal}} = \frac{1}{n} \sum \sum y_{ij.}^2 - y_{...}^2 / abn$$

$$SS_{AB} = SS_{\text{subtotal}} - SS_A - SS_B; \quad SS_E = \text{Subtraction}$$

$df_E > 0$  only if  $n > 1$ . When  $n = 1$ , no  $SS_E$  is available so we cannot test the effects. If we can assume that the interactions are negligible ( $(\tau\beta)_{ij} = 0$ ),  $MS_{AB}$  becomes a good estimate of  $\sigma^2$  and it can be used as  $MS_E$ . Caution: if the assumption is wrong, then error and interaction are confounded and testing results can go wrong.

## Battery Life Example

```
data battery;
input mat temp life;
datalines;
1 1 130
1 1 155
1 1 74
: : :
: : :
3 3 104
3 3 82
3 3 60
;

proc glm;
class mat temp;
model life=mat temp mat*temp;
output out=batnew r=res p=pred;
run;
```

Dependent Variable: life

Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model	8	59416.22222	7427.02778	11.00	<.0001
Error	27	18230.75000	675.21296		
Cor Total	35	77646.97222			

R-Square	Coeff Var	Root MSE	life Mean
0.765210	24.62372	25.98486	105.5278

Source	DF	Type I SS	Mean Square	F Value	Pr > F
mat	2	10683.72222	5341.86111	7.91	0.0020
temp	2	39118.72222	19559.36111	28.97	<.0001
mat*temp	4	9613.77778	2403.44444	3.56	0.0186

## Checking Assumptions

- 1 Errors are normally distributed

Histogram or QQplot of residuals

- 2 Constant variance

Residuals vs  $\hat{y}_{ij.}$  plot, Residuals vs factor A plot and Residuals vs factor B

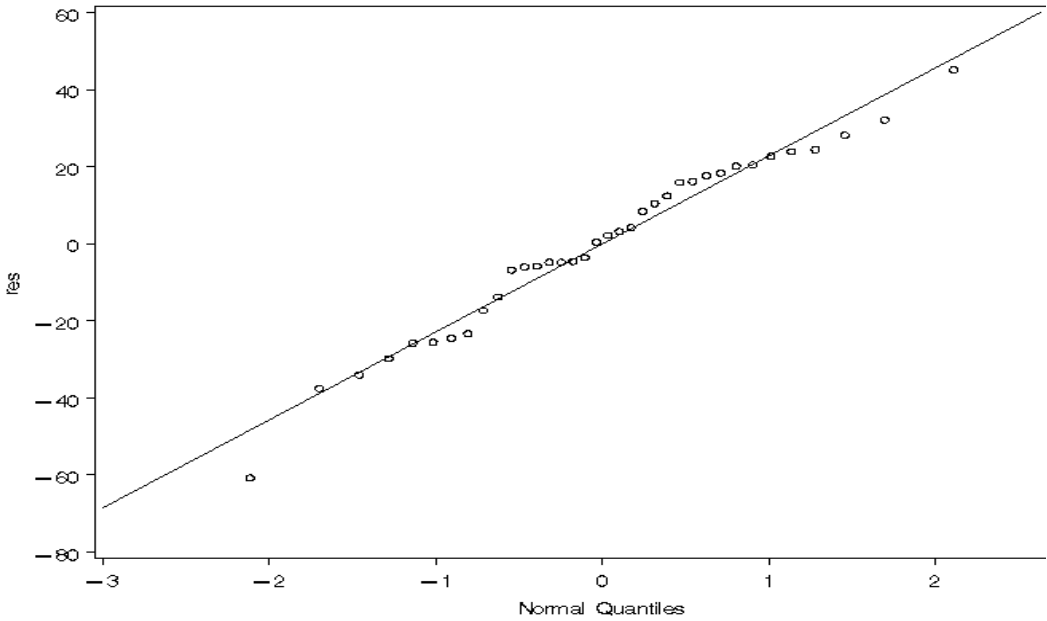
- 3 If  $n=1$ , no interaction.

Tukey's Test of Nonadditivity Assume  $(\tau\beta)_{ij} = \gamma\tau_i\beta_j$ .  $H_0 : \gamma = 0$ .

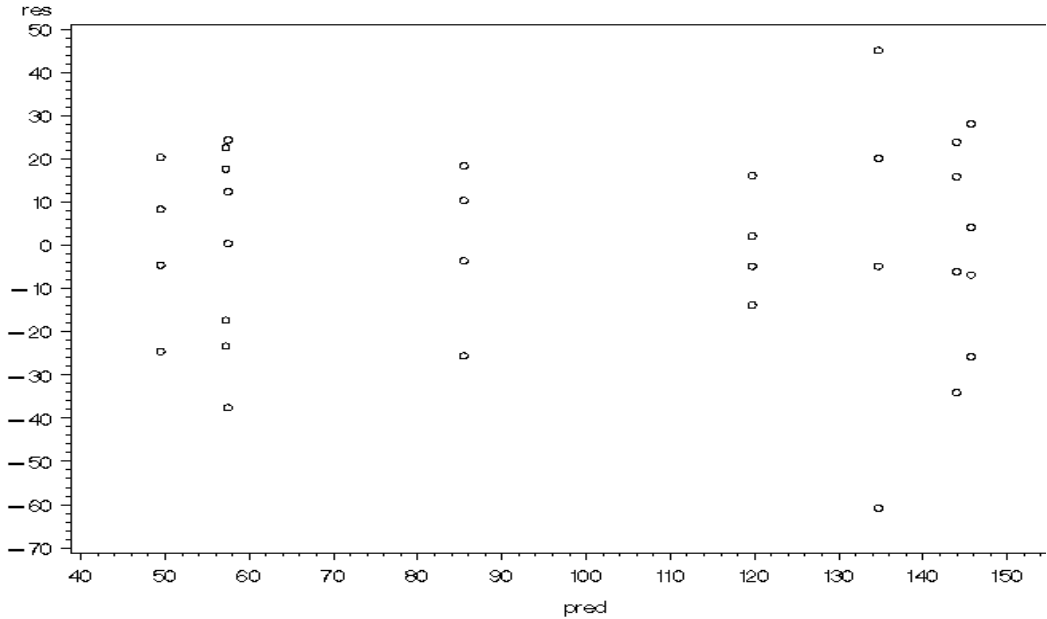
$$SS_N = \frac{[\sum \sum y_{ij} y_{i.} y_{.j} - y_{..} (SS_A + SS_B + y_{..}^2 / ab)]^2}{ab SS_A SS_B}$$

$$F_0 = \frac{SS_N / 1}{(SS_E - SS_N) / ((a - 1)(b - 1) - 1)} \sim F_{1, (a-1)(b-1)-1}$$

- the convenient procedure used for RCBD can be employed.







**Effects Estimation (Battery Experiment)**

0.  $\hat{\mu} = \bar{y}_{...} = 105.5278$

1. Treatment mean response, or cell mean, or predicted value,

$$\hat{y}_{ij} = \hat{\mu}_{ij} = \bar{y}_{ij.} = \hat{\mu} + \hat{\tau}_i + \hat{\beta}_j + (\hat{\tau\beta})_{ij}$$

	temperature		
material	1	2	3
1	134.75	57.25	57.50
2	155.75	119.75	49.50
3	144.00	145.75	85.50

2. Factor level means

row means  $\bar{y}_{i..}$  for  $A$ ; column means  $\bar{y}_{.j.}$  for  $B$ .

material :  $\bar{y}_{1..} = 83.166$ ,  $\bar{y}_{2..} = 108.3333$ ,  $\bar{y}_{3..} = 125.0833$

temperature :  $\bar{y}_{.1.} = 144.8333$ ,  $\bar{y}_{.2.} = 107.5833$ ,  $\bar{y}_{.3.} = 64.1666$

### 3. Main effects estimates

$$\hat{\tau}_1 = -22.3612, \hat{\tau}_2 = 2.8055, \hat{\tau}_3 = 19.555$$

$$\hat{\beta}_1 = 39.3055, \hat{\beta}_2 = 2.0555, \hat{\beta}_3 = -41.3611$$

### 4. Interactions $((\hat{\tau}\hat{\beta})_{ij})$

material	temperature		
	1	2	3
1	12.2779	-27.9721	15.6946
2	8.1112	9.3612	-17.4722
3	-20.3888	18.6112	1.7779

## Understanding Interactions

### Example I Data 1:

A B resp;

1 1 18

1 1 22

1 2 27

1 2 33

2 1 39

2 1 41

2 2 51

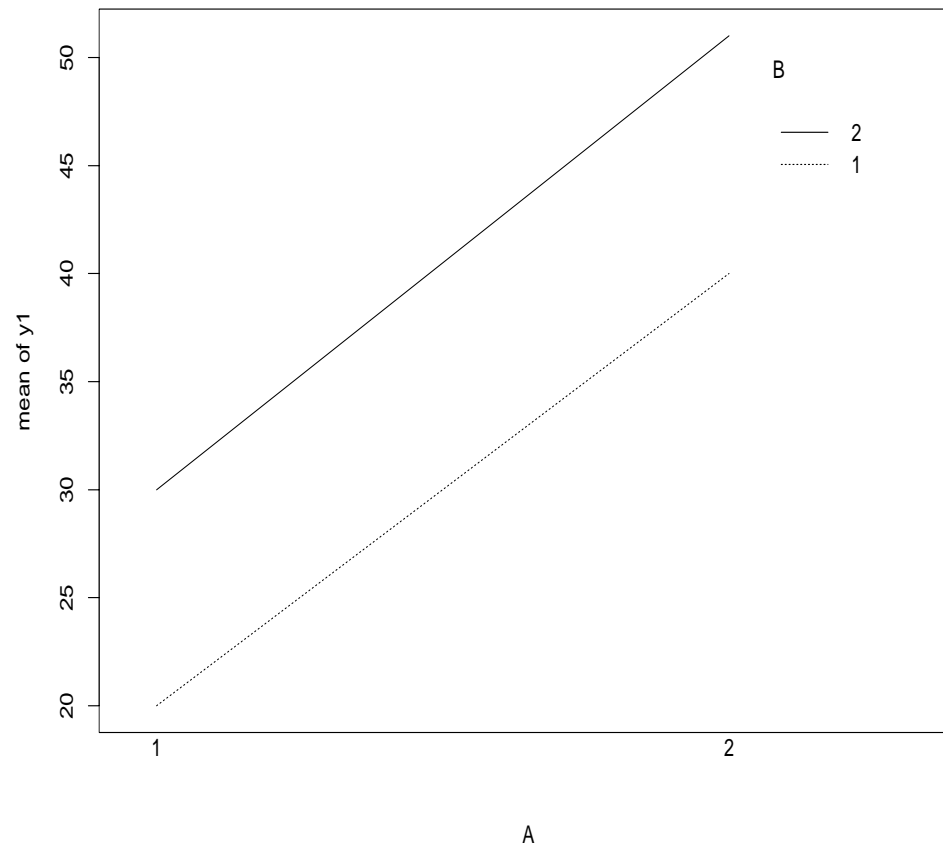
2 2 51

-----

Dependent Variable: resp

Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
A	1	840.5000000	840.5000000	120.07	0.0004
B	1	220.5000000	220.5000000	31.50	0.0050
A*B	1	0.5000000	0.5000000	0.07	0.8025
Error	4	28.0000000	7.0000000		
Cor Total	7	1089.5000000			

## Interaction plot for $A$ and $B$ (No Interaction)



Difference between level means of  $B$  (with  $A$  fixed at a level) does not depend on the level of  $A$ ; demonstrated by two parallel lines.

**Example I Data 2**

A B resp

1 1 19

1 1 21

1 2 38

1 2 42

2 1 53

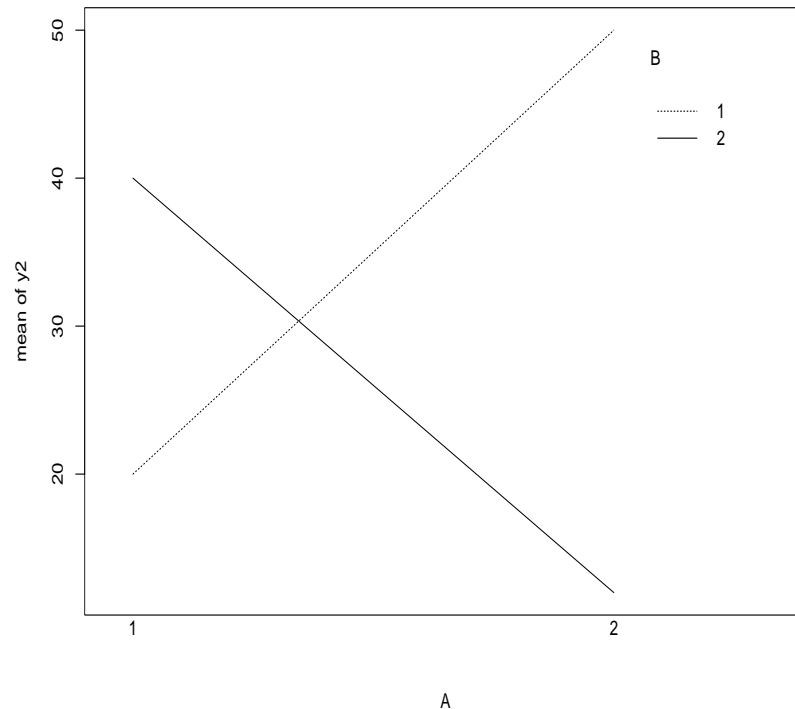
2 1 47

2 2 10

2 2 14

-----

Sum of					
Source	DF	Squares	Mean Square	F Value	Pr > F
A	1	2.000000	2.000000	0.22	0.6619
B	1	162.000000	162.000000	18.00	0.0132
A*B	1	1682.000000	1682.000000	186.89	0.0002
Error	4	36.000000	9.000000		
Cor Total	7	1882.000000			

**Interaction Plot for  $A$  and  $B$  (Antagonistic Interaction from  $B$  to  $A$ )**

Difference between level means of  $B$  (with  $A$  fixed at a level) depends on the level of  $A$ . If the trend of mean response over  $A$  reverses itself when  $B$  changes from one level to another, the interaction is said to be antagonistic from  $B$  to  $A$ . Demonstrated by two lines with slopes of opposite signs.

**Example I Data 3**

A B resp

1 1 21

1 1 21

1 2 27

1 2 33

2 1 62

2 1 67

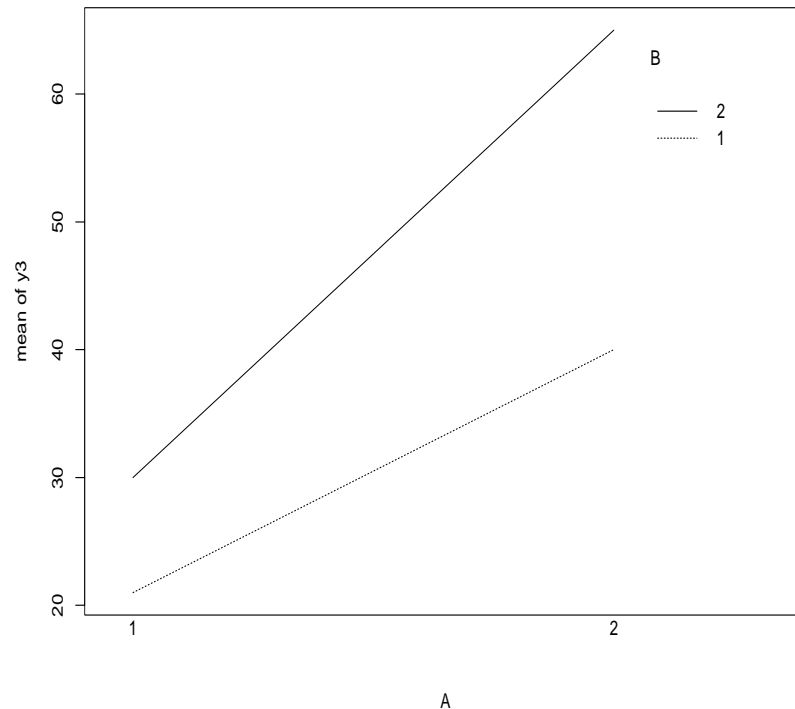
2 2 38

2 2 42

-----

		Sum of			
Source	DF	Squares	Mean Square	F Value	Pr > F
A	1	1431.125000	1431.125000	148.69	0.0003
B	1	120.125000	120.125000	12.48	0.0242
A*B	1	561.125000	561.125000	58.30	0.0016
Error	4	38.500000	9.625000		
Co Total	7	2150.875000			



**Interaction Plot for  $A$  and  $B$  (Synergistic Interaction from  $B$  to  $A$ )**

Difference between level means of  $B$  (with  $A$  fixed at a level) depends on the level of  $A$ . If the trend of mean response over  $A$  do not change when  $B$  changes from one level to another, the interaction is said to be synergistic; demonstrated by two unparallelled lines with slopes of the same sign.

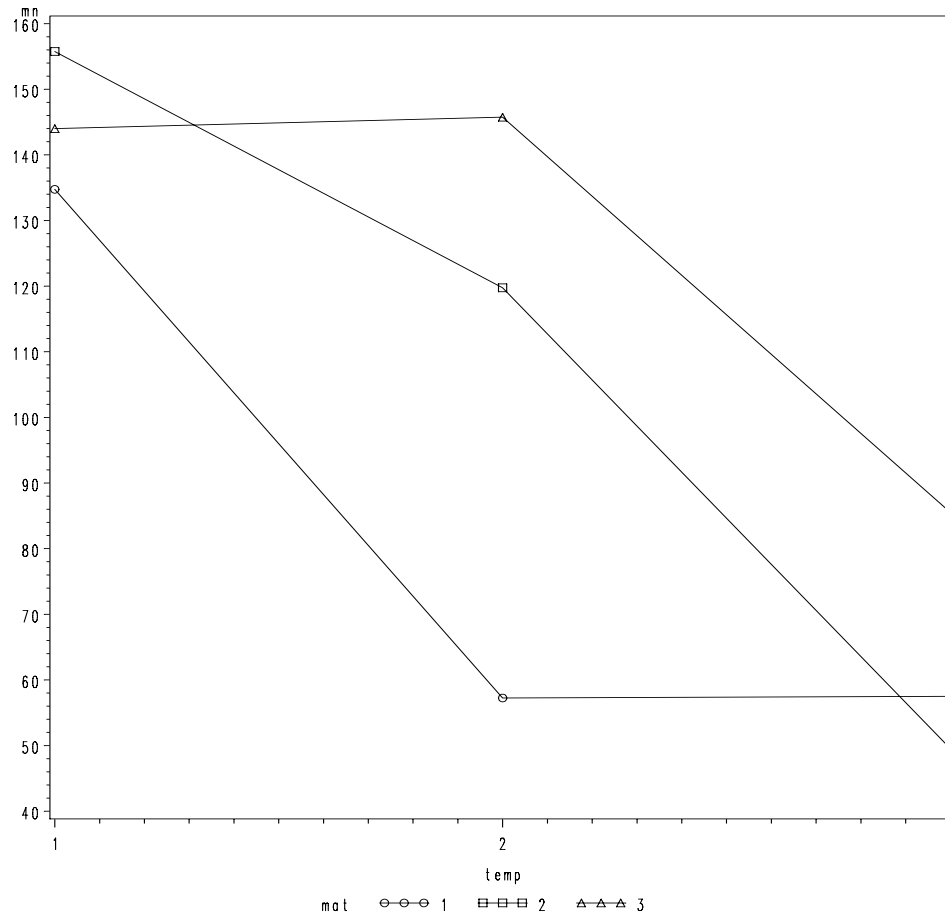
## Interaction Plot: Battery Experiment

```
data battery;
input mat temp life;
datalines;
1 1 130
.....
.....
3 3 60;

proc means noprint;
var life;
by mat temp;
output out=batterymean mean=mn;

symbol1 v=circle i=join;
symbol2 v=square i=join;
symbol3 v=triangle i=join;
proc gplot;
plot mn*temp=mat;
run;
```

## Interaction Plot for Material and Temperature



## Multiple comparison when factors don't interact

When factors don't interact, i.e., the  $F$  test for interaction is not significant in the ANOVA, factor level means can be compared to draw conclusions regarding their effects on response.

- $\text{Var}(\bar{y}_{i..}) = \frac{\sigma^2}{nb}$ ,  $\text{Var}(\bar{y}_{.j.}) = \frac{\sigma^2}{na}$

- 

For  $A$  or rows :  $\text{Var}(\bar{y}_{i..} - \bar{y}_{i'..}) = \frac{2\sigma^2}{nb}$ ; For  $B$  or columns :  $\text{Var}(\bar{y}_{.j.} - \bar{y}_{.j'.}) = \frac{2\sigma^2}{na}$

- Tukey's method

For rows:  $\text{CD} = \frac{q_{\alpha}(a, ab(n-1))}{\sqrt{2}} \sqrt{\text{MSE} \frac{2}{nb}}$

For columns:  $\text{CD} = \frac{q_{\alpha}(b, ab(n-1))}{\sqrt{2}} \sqrt{\text{MSE} \frac{2}{na}}$

- Bonferroni method:  $\text{CD} = t_{\alpha/2m, ab(n-1)} \text{S.E.}$ , where S.E. depends on whether for rows or columns.

### Level mean comparison when $A$ and $B$ interact: An Example

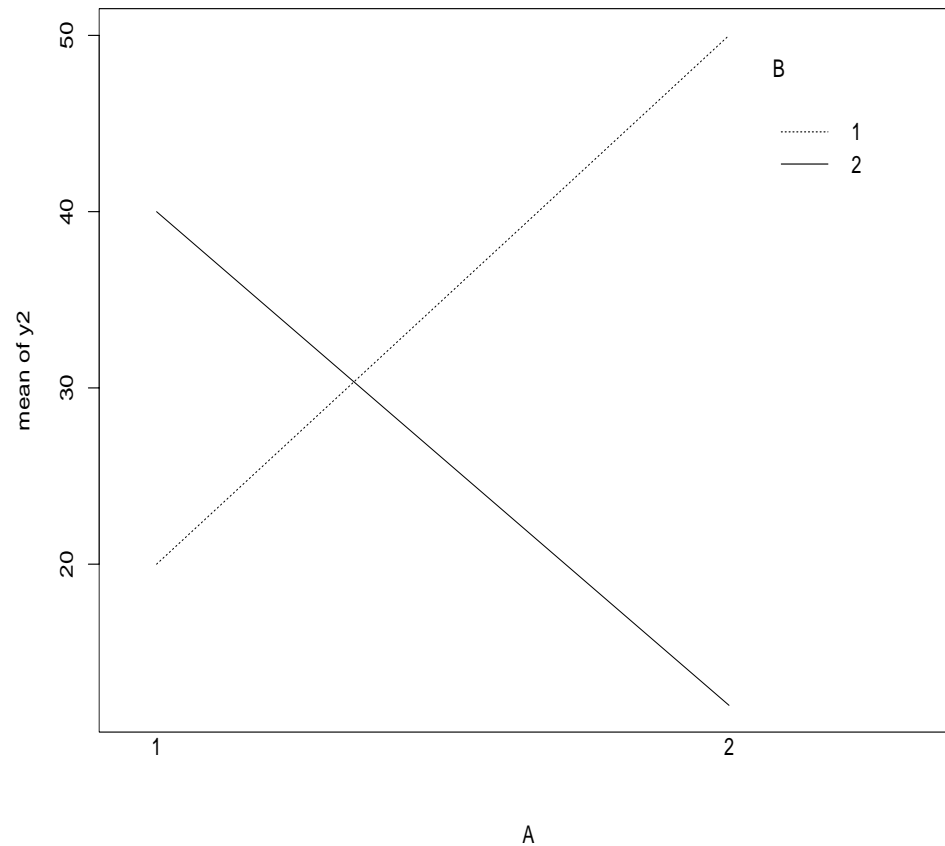
A	B	
	1	2
1	19, 21	38, 42
2	53, 47	10, 14

Compare factor level means of A:

$$\bar{y}_{1..} = (19 + 21 + 38 + 42)/4 = 30$$

$$\bar{y}_{2..} = (53 + 47 + 10 + 14)/4 = 31 = \bar{y}_{1..}$$

**Does Factor A have effect on the response?**



When interactions are present, be careful interpreting factor level means (row or column) comparisons because it can be misleading. Usually, we will directly compare treatment means (or cell means) instead.

## Multiple comparisons when factors interact: treatment (cell) mean comparison

When factors interact, multiple comparison is usually directly applied to treatment means

$$\mu_{ij} = \mu + \tau_i + \beta_j + (\tau\beta)_{ij} \text{ vs } \mu_{i'j'} = \mu + \tau_{i'} + \beta_{j'} + (\tau\beta)_{i'j'}$$

- $\hat{\mu}_{ij} = \bar{y}_{ij.}$  and  $\hat{\mu}_{i'j'} = \bar{y}_{i'j'.$
- $\text{Var}(\bar{y}_{ij.} - \bar{y}_{i'j'}.) = \frac{2\sigma^2}{n}$
- there are  $ab$  treatment means and  $m_0 = \frac{ab(ab-1)}{2}$  pairs.
- Tukey's method:

$$\text{CD} = \frac{q_{\alpha}(ab, ab(n-1))}{\sqrt{2}} \sqrt{\text{MSE} \frac{2}{n}}$$

- Bonferroni's method.

$$\text{CD} = t_{\alpha/2m, ab(n-1)} \sqrt{\text{MSE} \frac{2}{n}}$$

## SAS Code and Output

```
proc glm data=battery;  
class mat temp;  
model life=mat temp mat*temp;  
means mat|temp /tukey lines;  
lsmeans mat|temp/tdiff adjust=tukey;  
run;
```

=====

The GLM Procedure

Least Squares Means

Adjustment for Multiple Comparisons: Tukey

mat	life	LSMEAN	LSMEAN Number
1	83.166667		1
2	108.333333		2
3	125.083333		3



Least Squares Means for Effect mat  
t for  $H_0: \text{LSMean}(i) = \text{LSMean}(j)$  / Pr > |t|

Dependent Variable: life

i/j	1	2	3
1		-2.37236 0.0628	-3.95132 0.0014
2	2.372362 0.0628		-1.57896 0.2718
3	3.951318 0.0014	1.578956 0.2718	

**Output (continued)**

Least Squares Means

Adjustment for Multiple Comparisons: Tukey

		LSMEAN	
temp	life	LSMEAN	Number
1		144.833333	1
2		107.583333	2
3		64.166667	3

Least Squares Means for Effect temp

t for  $H_0: \text{LSMean}(i) = \text{LSMean}(j)$  / Pr > |t|

Dependent Variable: life

i/j	1	2	3
1		3.51141	7.604127
		0.0044	<.0001
2	-3.51141		4.092717
	0.0044		0.0010
3	-7.60413	-4.09272	
	<.0001	0.0010	

**Output (continued)**

The GLM Procedure

Least Squares Means

Adjustment for Multiple Comparisons: Tukey

			LSMEAN
mat	temp	life	LSMEAN
1	1	134.750000	1
1	2	57.250000	2
1	3	57.500000	3
2	1	155.750000	4
2	2	119.750000	5
2	3	49.500000	6
3	1	144.000000	7
3	2	145.750000	8
3	3	85.500000	9

**Output**

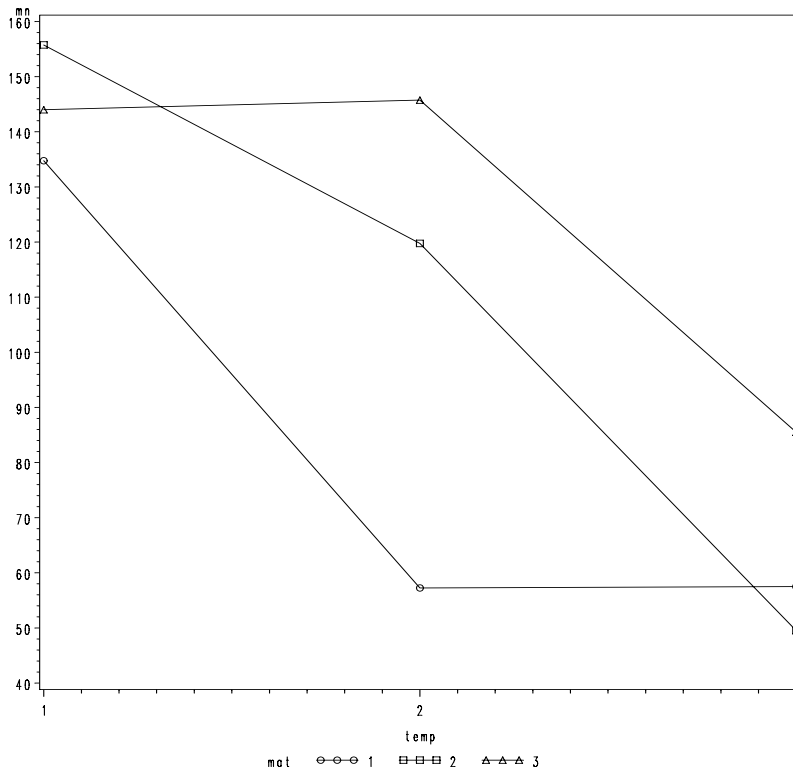
i / j	1	2	3	4	5
1		4.2179 0.0065	4.204294 0.0067	-1.14291 0.9616	0.816368 0.9953
2	-4.2179 0.0065		-0.01361 1.0000	-5.36082 0.0003	-3.40153 0.0460
3	-4.20429 0.0067	0.013606 1.0000		-5.34721 0.0004	-3.38793 0.0475
4	1.142915 0.9616	5.360815 0.0003	5.347209 0.0004		1.959283 0.5819
5	-0.81637 0.9953	3.401533 0.0460	3.387926 0.0475	-1.95928 0.5819	
6	-4.63969 0.0022	-0.42179 1.0000	-0.4354 1.0000	-5.78261 0.0001	-3.82332 0.0172
7	0.503427 0.9999	4.721327 0.0018	4.707721 0.0019	-0.63949 0.9991	1.319795 0.9165
8	0.59867 0.9995	4.81657 0.0014	4.802964 0.0015	-0.54425 0.9997	1.415038 0.8823
9	-2.68041 0.2017	1.537493 0.8282	1.523887 0.8347	-3.82332 0.0172	-1.86404 0.6420

**Output (continued)**

i / j	6	7	8	9
1	4.63969 0.0022	-0.50343 0.9999	-0.59867 0.9995	2.680408 0.2017
2	0.42179 1.0000	-4.72133 0.0018	-4.81657 0.0014	-1.53749 0.8282
3	0.435396 1.0000	-4.70772 0.0019	-4.80296 0.0015	-1.52389 0.8347
4	5.782605 0.0001	0.639488 0.9991	0.544245 0.9997	3.823323 0.0172
5	3.823323 0.0172	-1.31979 0.9165	-1.41504 0.8823	1.86404 0.6420
6		-5.14312 0.0006	-5.23836 0.0005	-1.95928 0.5819
7	5.143117 0.0006		-0.09524 1.0000	3.183834 0.0743
8	5.23836 0.0005	0.095243 1.0000		3.279077 0.0604
9	1.959283 0.5819	-3.18383 0.0743	-3.27908 0.0604	

## Fitting Response Curves or Surfaces

Battery Experiment:



Goal: Model the functional relationship between lifetime and temperature at every material level.

- Material is qualitative while temperature is quantitative
- Want to fit the response using effects of material, temperature and their interactions
- Temperature has quadratic effect. Could use orthogonal polynomials as before. Here we will simply  $t$  and  $t^2$ .
- Levels of material need to be converted to dummy variables denoted by  $x_1$  and  $x_2$  as follows.

mat	$x_1$	$x_2$
1	1	0
2	0	1
3	-1	-1

- For convenience, convert temperature to -1,0 and 1 using

$$t = \frac{\text{temperature} - 70}{55}$$

**Fitting Response Curve: Model matrix**

mat	temp	==>	x1	x2	t	t^2	x1*t	x2*t	x1*t^2	x2*t^2
1	15		1	0	-1	1	-1	0	1	0
1	70		1	0	0	0	0	0	0	0
1	125		1	0	1	1	1	0	1	0
2	15		0	1	-1	1	0	1	0	1
2	70		0	1	0	0	0	0	0	0
2	125		0	1	1	1	0	-1	0	1
3	15		-1	-1	-1	1	1	-1	-1	-1
3	70		-1	-1	0	0	0	0	0	0
3	125		-1	-1	1	1	-1	1	-1	-1

The following model is used:

$$y_{ijk} = \beta_0 + \beta_1 x_1 + \beta_2 x_2 + \beta_3 t + \beta_4 x_1 t + \beta_5 x_2 t + \beta_6 t^2 + \beta_7 x_1 t^2 + \beta_8 x_2 t^2 + \epsilon_{ijk}$$

Want to estimate the coefficients:  $\beta_0, \beta_1, \beta_2, \dots, \beta_8$  using regression



## SAS Code: Battery Life Experiment

```
data life;
  input mat temp y @@;
  if mat=1 then x1=1;
  if mat=1 then x2=0;
  if mat=2 then x1=0;
  if mat=2 then x2=1;
  if mat=3 then x1=-1;
  if mat=3 then x2=-1;
  t=(temp-70)/55;
  t2=t*t; x1t=x1*t;  x2t=x2*t;
  x1t2=x1*t2;  x2t2=x2*t2;
datalines;
1 15 130 1 15 155 1 70 34 1 70 40 1 125 20 1 125 70
1 15 74 1 15 180 1 70 80 1 70 75 1 125 82 1 125 58
2 15 150 2 15 188 2 70 136 2 70 122 2 125 25 2 125 70
2 15 159 2 15 126 2 70 106 2 70 115 2 125 58 2 125 45
3 15 138 3 15 110 3 70 174 3 70 120 3 125 96 3 125 104
3 15 168 3 15 160 3 70 150 3 70 139 3 125 82 3 125 60
;
proc reg;
  model y=x1 x2 t x1t x2t t2 x1t2 x2t2;
run;
```

**SAS output**

## Analysis of Variance

Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model	8	59416	7427.02778	11.00	<.0001
Error	27	18231	675.21296		
CorrectedTotal	35	77647			

## Parameter Estimates

Variable	DF	Parameter Estimate	Standard Error	t Value	Pr >  t
Intercept	1	107.58333	7.50118	14.34	<.0001
x1	1	-50.33333	10.60827	-4.74	<.0001
x2	1	12.16667	10.60827	1.15	0.2615
t	1	-40.33333	5.30414	-7.60	<.0001
x1t	1	1.70833	7.50118	0.23	0.8216
x2t	1	-12.79167	7.50118	-1.71	0.0996
t2	1	-3.08333	9.18704	-0.34	0.7398
x1t2	1	41.95833	12.99243	3.23	0.0033
x2t2	1	-14.04167	12.99243	-1.08	0.2894

## Results

From the SAS output, the fitted model is

$$\begin{aligned}\hat{y} = & 107.58 - 50.33x_1 - 12.17x_2 - 40.33t + 1.71x_1t - 12.79x_2t \\ & - 3.08t^2 + 41.96x_1t^2 - 14.04x_2t^2\end{aligned}$$

Note that terms with insignificant coefficients are still kept in the fitted model here. In practice, model selection may be employed to remove unimportant terms and choose the best fitted model. But we will not pursue it in this course.

The model above are in terms of both  $x_1$ ,  $x_2$  and  $t$ . We can specify the level of material, that is, the values of dummy variable  $x_1$  and  $x_2$ , to derive fitted response curves for material at different levels.

## Fitted Response Curves

Three response curves:

- Material at level 1 ( $x_1 = 1, x_2 = 0$ )

$$E(y_{1t}) = 57.25 - 38.62t + 38.88t^2$$

- Material at level 2 ( $x_1 = 0, x_2 = 1$ )

$$E(y_{2t}) = 119.75 - 53.12t - 17.12t^2$$

- Material at level 3 ( $x_1 = -1, x_2 = -1$ )

$$E(y_{3t}) = 145.74 - 29.25t - 31t^2$$

Where  $t = \frac{\text{temperature} - 70}{55}$ .

These curves can be used to predict lifetime of battery at any temperature between 15 and 125 degree. But one needs to be careful about extrapolation. For example, the fitted curve at Material level 1 suggests that lifetime of a battery can be infinity when temperature goes to infinity, which is clearly false.

## General Factorial Design and Model

- Factorial Design - including all possible level combinations
- $a$  levels of Factor  $A$ ,  $b$  levels of Factor  $B$ , . . .
- (Straightforward ANOVA if all **fixed effects**)
- In 3 factor model  $\rightarrow nabc$  observations
- Need  $n > 1$  to test for all possible interactions
- Statistical Model (3 factor)

$$y_{ijkl} = \mu + \tau_i + \beta_j + \gamma_k + (\tau\beta)_{ij} + (\beta\gamma)_{jk} + (\tau\gamma)_{ik} + (\tau\beta\gamma)_{ijk} + \epsilon_{ijkl}$$

$$\left\{ \begin{array}{l} i = 1, 2, \dots, a \\ j = 1, 2, \dots, b \\ k = 1, 2, \dots, c \\ l = 1, 2, \dots, n \end{array} \right.$$

## Analysis of Variance Table

Source of Variation	Sum of Squares	Degrees of Freedom	Mean Square	$F_0$
Factor A	$SS_A$	$a - 1$	$MS_A$	$F_0$
Factor B	$SS_B$	$b - 1$	$MS_B$	$F_0$
Factor C	$SS_C$	$c - 1$	$MS_C$	$F_0$
AB	$SS_{AB}$	$(a - 1)(b - 1)$	$MS_{AB}$	$F_0$
AC	$SS_{AC}$	$(a - 1)(c - 1)$	$MS_{AC}$	$F_0$
BC	$SS_{BC}$	$(b - 1)(c - 1)$	$MS_{BC}$	$F_0$
ABC	$SS_{ABC}$	$(a - 1)(b - 1)(c - 1)$	$MS_{ABC}$	$F_0$
Error	$SS_E$	$abc(n - 1)$	$MS_E$	
Total	$SS_T$	$abcn - 1$		

## Bottling Experiment: SAS Code

```
option nocenter
data bottling;
input carb pres spee devi;
datalines;
1 1 1 -3
1 1 1 -1
1 1 2 -1
1 1 2 0
: : : :
3 2 1 9
3 2 2 10
3 2 2 11
;
proc glm;
class carb pres spee;
model devi=carb|pres|spee;
run;
```

**Bottling Experiment: SAS Output**

Dependent Variable: devi

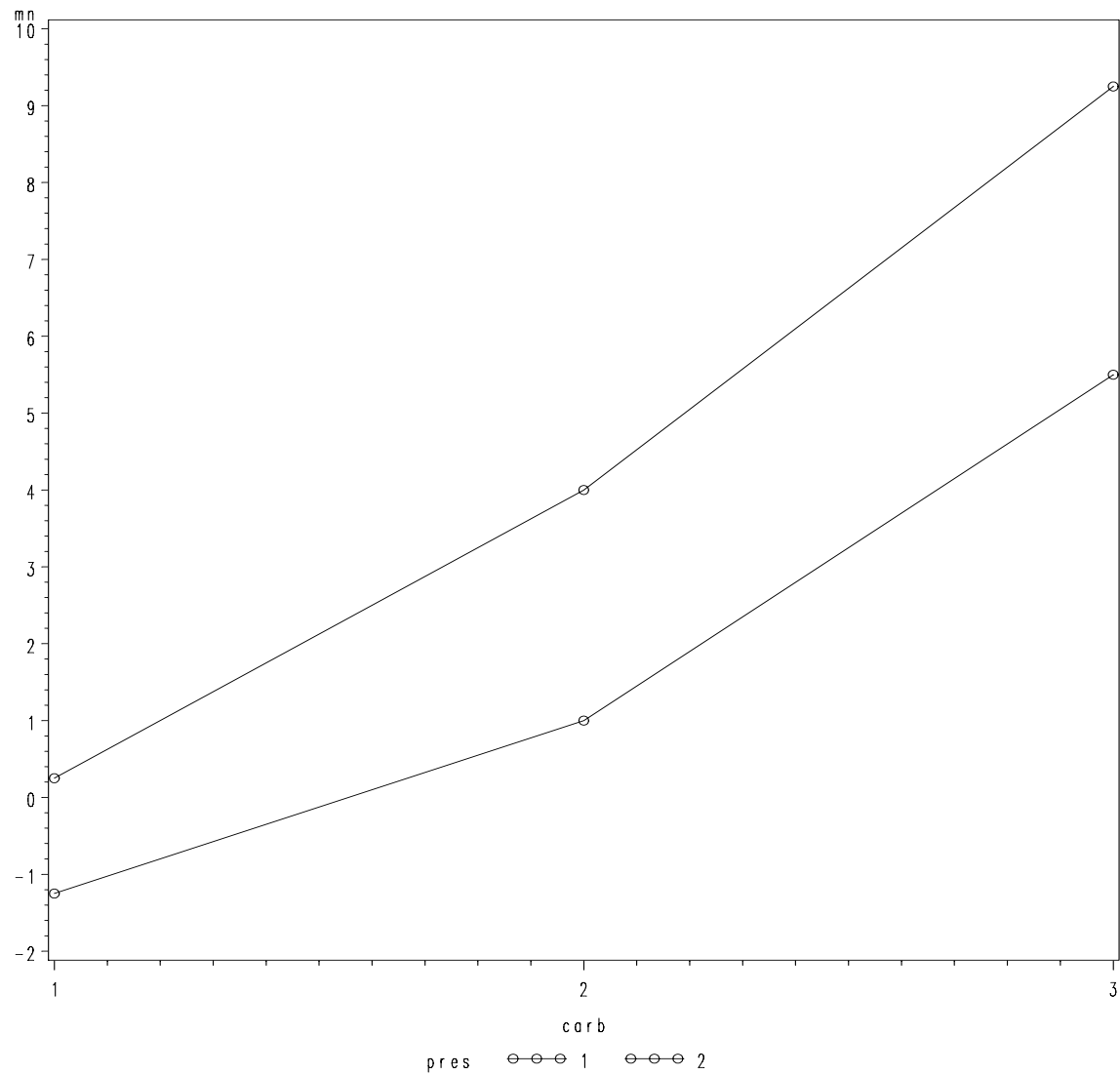
Source	DF	Sum of Squares	Mean Square	F Value	Pr > F
Model	11	328.1250000	29.8295455	42.11	<.0001
Error	12	8.5000000	0.7083333		
Co Total	23	336.6250000			

R-Square	Coeff Var	Root MSE	devi Mean
0.974749	26.93201	0.841625	3.125000

Source	DF	Type I SS	Mean Square	F Value	Pr > F
carb	2	252.7500000	126.3750000	178.41	<.0001
pres	1	45.3750000	45.3750000	64.06	<.0001
carb*pres	2	5.2500000	2.6250000	3.71	0.0558
spee	1	22.0416667	22.0416667	31.12	0.0001
carb*spee	2	0.5833333	0.2916667	0.41	0.6715
pres*spee	1	1.0416667	1.0416667	1.47	0.2486
carb*pres*spee	2	1.0833333	0.5416667	0.76	0.4869



## Interaction Plot for Carb and Pressure



### **General Factorial Model**

- Usual assumptions and diagnostics
- Multiple comparisons: simple extensions of the two-factor case
- Often higher order interactions are negligible.
- Beyond three-way interactions difficult to picture.
- Pooled together with error (increase  $df_E$ )

## **Blocking in Factorial Design: Example**

### **Battery Life Experiment:**

An engineer is studying the effective lifetime of some battery. Two factors, plate material and temperature, are involved. There are three types of plate materials (1, 2, 3) and three temperature levels (15, 70, 125). Four batteries are tested at each combination of plate material and temperature, and all 36 tests are run in random order. The experiment and the resulting observed battery life data are given below.

material	temperature		
	15	70	125
1	130,155,74,180	34,40,80,75	20,70,82,58
2	150,188,159,126	136,122,106,115	25,70,58,45
3	138,110,168,160	174,120,150,139	96,104,82,60

**If we assume further that four operators (1,2,3,4) were hired to conduct the experiment. It is known that different operators can cause systematic difference in battery lifetime. Hence operators should be treated as blocks**

**The blocking scheme is every operator conduct a single replicate of the full factorial design**

**For each treatment (treatment combination), the observations were in the order of the operators 1, 2, 3, and 4.**

This is a blocked factorial design

## Statistical Model for Blocked Factorial Experiment

$$y_{ijk} = \mu + \tau_i + \beta_j + (\tau\beta)_{ij} + \delta_k + \epsilon_{ijk}$$

$i = 1, 2, \dots, a$ ,  $j = 1, 2, \dots, b$  and  $k = 1, 2, \dots, n$ ,  $\delta_k$  is the effect of the  $k$ th block.

- randomization restriction is imposed. (complete block factorial design).
- interactions between blocks and treatment effects are assumed to be negligible.
- The previous ANOVA table for the experiment should be modified as follows:  
Add: Block Sum of Square

$$SS_{Blocks} = \frac{1}{ab} \sum_k y_{..k}^2 - \frac{y_{...}^2}{abn} \text{ D.F. } n - 1$$

Modify: Error Sum of Squares:

$$(\text{new})SS_E = (\text{old})SS_E - SS_{Blocks} \text{ D.F. } (ab - 1)(n - 1)$$

- other inferences should be modified accordingly.

## SAS Code and Output

```
data battery;
input mat temp oper life;
dataline;
1 1 1 130
.....
.....
3 3 4 60
;
proc glm;
class mat temp oper;
model life=oper mat|temp;
output out=new1 r=resi p=pred;
```

=====

Dependent Variable: life

		Sum of			
Source	DF	Squares	Mean Square	F Value	Pr > F
Model	11	59771.19444	5433.74495	7.30	<.0001
Error	24	17875.77778	744.82407		
CorTotal	35	77646.97222			
Source	DF	Type I SS	Mean Square	F Value	Pr > F
oper	3	354.97222	118.32407	0.16	0.9229
mat	2	10683.72222	5341.86111	7.17	0.0036
temp	2	39118.72222	19559.36111	26.26	<.0001
mat*temp	4	9613.77778	2403.44444	3.23	0.0297

## Factorial Experiment with Two blocking factors

Use Latin square as blocking scheme

1. Suppose the experimental factors are F1 and F2. A has three levels (1,2, 3) and B has 2 levels. There are  $3 \times 2 = 6$  treatment combinations. These treatments can be represented by Latin letters

F1	F2	Treatment
1	1	A
1	2	B
2	1	C
2	2	D
3	1	E
3	2	F



Two blocking factors are Block1 and Block2, each with 6 blocks.

2. A  $6 \times 6$  Latin square can be used as the blocking scheme:

		Block1					
Block2		1	2	3	4	5	6
1		A	B	C	D	E	F
2		B	C	D	E	F	A
3		C	D	E	F	A	B
4		D	E	F	A	B	C
5		E	F	A	B	C	D
6		F	A	B	C	D	E

3. Statistical Model

$$y_{ijkl} = \mu + \alpha_i + \tau_j + \beta_k + (\tau\beta)_{jk} + \theta_l + \epsilon_{ijkl}$$

where,  $\alpha_i$  and  $\theta_l$  are blocking effects,  $\tau_j$ ,  $\beta_k$  and  $(\tau\beta)_{jk}$  are the treatment main effects and interactions